

# Availability Analysis of Filler System in a Process Industry (Brewary Plant)

Sunil kadiyan<sup>1</sup>, Seeone Sharma<sup>2</sup>, Raju<sup>3</sup>, Rajesh Gautam<sup>4</sup>

**Abstract:** The most of the systems in the industries are complex and repairable. If we wish to achieve the optimum performance of the system then we need to understand the Reliability, Availability and maintenance (RAM) parameters. In this paper we discuss the availability of Filler system in brewery plant by using the concept of mathematical modeling. Markov Birth Death process is used to find out all the probabilities of the systems and the subsystems. These probabilities are full working, reduced and failure state. After understanding the layout of the packaging department, draw transition diagram for various subsystems then differential equations and Steady state probabilities are determined. By taking data from the log table available in the industry about the failure rate and repair rate of various systems and sub-systems the decision matrix are developed by using MATLAB programming. This gives availability for various combinations of failure rate and repair rate of all sub-systems. Graphs between availability and failure rate and availability and repair rate suggest the availability is decreases as the failure rate increases and availability is increases as the repair rate increase.

**Keywords:** Reliability, Availability, Mean Time to Failure, Mean Time between Failures, Steady state probabilities, Performance.

## 1. INTRODUCTION

The filler system consist of six sub systems A, B, C, D, E, F in series and the subsystem A also worked in reduced capacity. Where A=Conveyer belt speed, B=Sensor Assembly, C= Star Wheel, D=Rotary Filler, E= Rotary Cork Assembly, F=Conveyer Belt. According to Jai Singh et al. (19 April, 1994), The Availability of a system can be improved by using the standby units of limited subsystems, where the chances of failure is high.

According to Navneet Arora et al.(19 May 1995), the availability analysis of a steam generation system consisting of three subsystems A, B and D and a power generation system consisting of four subsystems E, F, G and H arranged in series, with three states i.e. good, reduced and failed. Taking constant failure and repair rates for each working unit, the mathematical formulation is done using the Birth-Death process. Expressions for steady state availability and the MTBF (mean time between failures) are derived. The graphs are given, depicting the effect of failure and repair rates on the system availability. The results are supplied to the plant personnel, to plan the policies for failure free running of the systems for a long duration.

### Assumptions



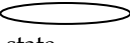
1. At any given time the system is either in operating state or in the failed state.
2. Failure rate and repair rate are constant.
3. A repaired sub system is as good as new.
4. Standby sub systems are of the same nature and capacity as the active sub system.

5. In subsystem A, standby unit is always available when online unit fails.

### The Most appropriate Approaches used for reliability estimation are

1. Monte-Carlo Simulation Technique.
2. The Markov Process Approach.
3. Failure Modes and Effects Analysis(FMEA).
4. Reliability Block Diagrams (RBD).
5. Functional Logic Diagrams.
6. The Structure Function Approach.
7. Fault tree Analysis.
8. Event tree Analysis.

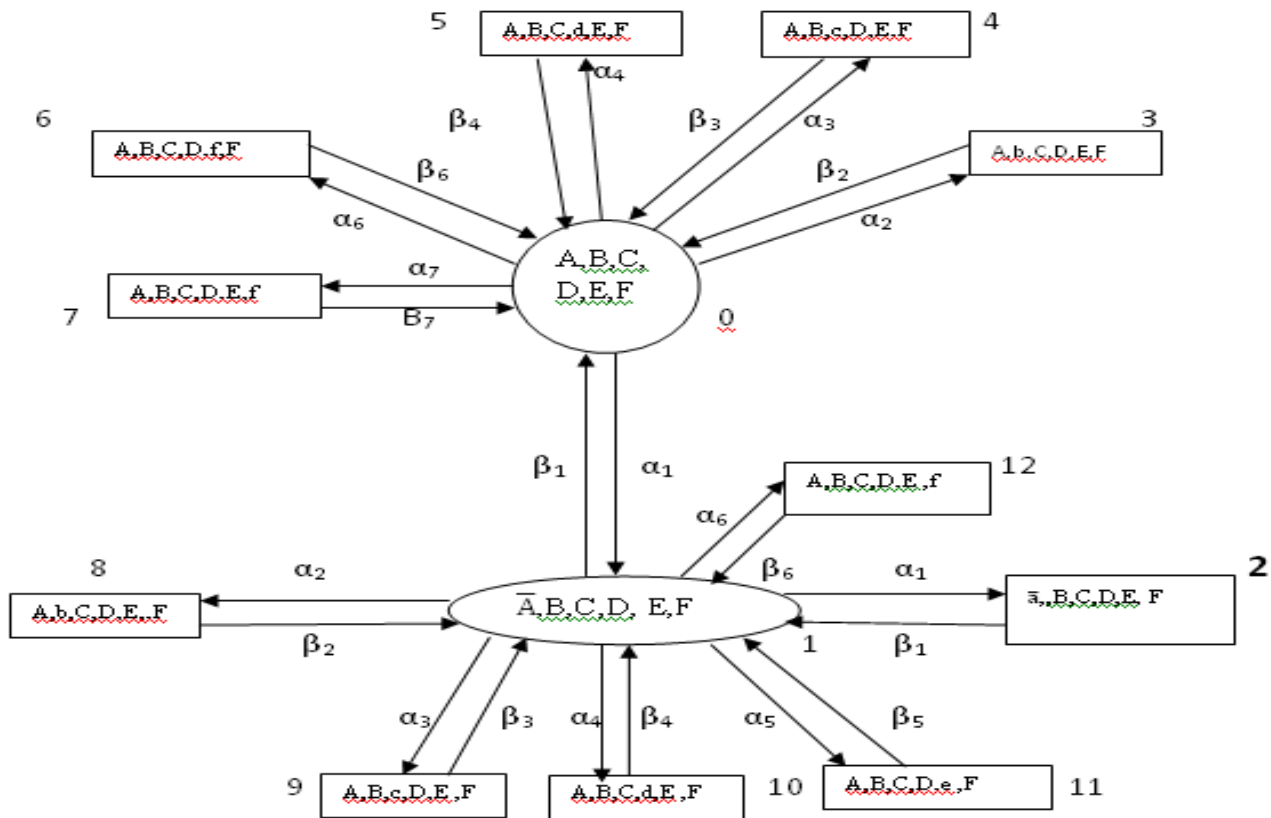
### Notations

1.  Indicate the system in operating condition.
2.  Indicates the system in fail condition.
3.  Indicates the system in reduced capacity state.
4. A, B, C, D, E, F indicate the subsystems are working at full capacity.
5.  $\bar{A}$  indicates that the subsystem is working at reduced capacity.
6. a,b,c,d,e,f indicates that all subsystems are in failed state.
7.  $\alpha_1$  Failure Rate of subsystem A
8.  $\alpha_2$  Failure Rate of subsystem B
9.  $\alpha_3$  Failure Rate of subsystem C
10.  $\alpha_4$  Failure Rate of subsystem D
11.  $\alpha_5$  Failure Rate of subsystem E
12.  $\alpha_6$  Failure Rate of subsystem F
13.  $\beta_1$  Repair Rate of subsystem A
14.  $\beta_2$  Repair Rate of subsystem B
15.  $\beta_3$  Repair Rate of subsystem C

16.  $\beta_4$  Repair Rate of subsystem D
17.  $\beta_5$  Repair Rate of subsystem E
18.  $\beta_6$  Repair Rate of subsystem F
19.  $d/dt$  indicates derivative w.r.t. 't'.
20.  $P_0(t)$  denotes the probability that at time  $t$  all units are working.
21.  $P_1(t)$  denotes the probability that at time  $t$  the system is in reduced capacity state due to failure of subsystem A.
22.  $P_2(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem A.
23.  $P_3(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem B.
24.  $P_4(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem C.
25.  $P_5(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem D.
26.  $P_6(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem E.

27.  $P_7(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem F.
28.  $P_8(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem B. and subsystem A working within reduced capacity.
29.  $P_9(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem C. and subsystem A working within reduced capacity.
30.  $P_{10}(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem D. and subsystem A working within reduced capacity.
31.  $P_{11}(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem E. and subsystem A working within reduced capacity.
32.  $P_{12}(t)$  denotes the probability that at time  $t$  the system is in failed state due to failure of subsystem F. and subsystem A working within reduced capacity.

### Transition Diagram:



Performance modeling of Filler System:

$$\begin{aligned} (d/dt + \alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6)P_0(t) &= \beta_1P_1(t) + \beta_2P_3(t) + \beta_3P_4(t) + \beta_4P_5(t) + \beta_5P_6(t) + \beta_6P_7(t) \dots (1) \\ (d/dt + \alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6 + \beta_1)P_1(t) &= \beta_1P_2(t) + \beta_2P_8(t) + \beta_3P_9(t) + \beta_4P_{10}(t) + \beta_5P_{11}(t) + \beta_6P_{12}(t) + \alpha_1P_0(t) \dots (2) \\ (d/dt + \beta_2)P_3(t) &= \alpha_2P_0(t) \dots (3) \\ (d/dt + \beta_1)P_2(t) &= \alpha_1P_1(t) \dots (4) \end{aligned}$$

$$\begin{aligned} (d/dt + \beta_3)P_4(t) &= \alpha_3P_0(t) \dots (5) \\ (d/dt + \beta_4)P_5(t) &= \alpha_4P_0(t) \dots (6) \\ (d/dt + \beta_5)P_6(t) &= \alpha_5P_0(t) \dots (7) \\ (d/dt + \beta_6)P_7(t) &= \alpha_6P_0(t) \dots (8) \\ (d/dt + \beta_2)P_8(t) &= \alpha_2P_1(t) \dots (9) \\ (d/dt + \beta_3)P_9(t) &= \alpha_3P_1(t) \dots (10) \\ (d/dt + \beta_4)P_{10}(t) &= \alpha_4P_1(t) \dots (11) \\ (d/dt + \beta_5)P_{11}(t) &= \alpha_5P_1(t) \dots (12) \end{aligned}$$

$$(d/dt + \beta_6)P_{12}(t) = \alpha_6 P_1(t) \dots (13)$$

With initial conditions at time  $t = 0$

$$P_i(t) = 1 \text{ for } i=0 \\ = 0 \text{ for } i \neq 0$$

Steady state availability of Filler Machine:

By putting  $d/dt = 0$  at  $t \rightarrow \infty$  in equations (1 to 13), the steady state probabilities are given as:-

$$P_3 = \alpha_2 / \beta_2 P_0 \dots (14)$$

$$P_2 = \alpha_1 / \beta_1 P_0 \dots (15)$$

$$P_4 = \alpha_3 / \beta_3 P_0 \dots (16)$$

$$P_5 = \alpha_4 / \beta_4 P_0 \dots (17)$$

$$P_6 = \alpha_5 / \beta_5 P_0 \dots (18)$$

$$P_7 = \alpha_6 / \beta_6 P_0 \dots (19)$$

$$P_8 = \alpha_2 / \beta_2 P_1 \dots (20)$$

$$P_9 = \alpha_3 / \beta_3 P_1 \dots (21)$$

$$P_{10} = \alpha_4 / \beta_4 P_1 \dots (22)$$

$$P_{11} = \alpha_5 / \beta_5 P_1 \dots (23)$$

$$P_{12} = \alpha_6 / \beta_6 P_1 \dots (24)$$

$$P_0 = \beta_1 P_1 + \beta_2 P_3 + \beta_3 P_4 + \beta_4 P_5 + \beta_5 P_6 + \beta_6 P_7 / (\alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6) \dots (25)$$

$$P_1 = \beta_1 P_2 + \beta_2 P_8 + \beta_3 P_9 + \beta_4 P_{10} + \beta_5 P_{11} + \beta_6 P_{12} + \alpha_1 P_0 / (\alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6 + \beta_1) \dots (26)$$

Put the values of  $P_1, P_2, P_4, P_5, P_6, P_7$ , in equation no. 25 and find the value of  $P_0$

$$P_0 = \beta_1 P_1 + \beta_2 P_2 + \beta_3 P_4 + \beta_4 P_5 + \beta_5 P_6 + \beta_6 P_7 / (\alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6)$$

$$(A-C) P_0 = \beta_1 P_1$$

$$P_0 = \beta_1 P_1 / (A-C)$$

$$F = \alpha_1 / (B-A)$$

$$G = (1 + \alpha_1 / \beta_1 + \alpha_2 / \beta_2 + \alpha_3 / \beta_3 + \alpha_4 / \beta_4 + \alpha_5 / \beta_5 + \alpha_6 / \beta_6)$$

$$H = (\alpha_2 / \beta_2 + \alpha_3 / \beta_3 + \alpha_4 / \beta_4 + \alpha_6 / \beta_6 + \alpha_5 / \beta_5)$$

Availability = Sum of probability of working state/ reduced state

$$P_0 = EP_1 \dots (27)$$

Put the values of  $P_2, P_8, P_9, P_{10}, P_{11}, P_{12}, P_0$ , in equation no. 26 and find the value of  $P_1$

$$P_1 = \beta_1 P_2 + \beta_2 P_8 + \beta_3 P_9 + \beta_4 P_{10} + \beta_5 P_{11} + \beta_6 P_{12} + \alpha_1 P_0 / (\alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6 + \beta_1)$$

$$P_1 = \{(\alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6) P_1 + \alpha_1 P_0\} / B$$

$$(B-A) P_1 = \alpha_1 P_0$$

$$P_1 = \alpha_1 P_0 / (B-A)$$

$$P_1 = FP_0 \dots (28)$$

The probability of full working/reduced state is determined by using normalizing conditions i.e. sum of the probabilities of all working states and failed states is equal to 1.

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$$\sum P_i = 1$$

$$i=0$$

$$P_0 + P_1 + P_2 + P_3 + P_4 + P_5 + P_6 + P_7 + P_8 + P_9 + P_{10} + P_{11} + P_{12} = 1$$

$$P_0 (1 + FG + H) = 1$$

$$P_0 = 1 / (1 + FG + H)$$

$$P_1 = F / (1 + FG + H)$$

$$\text{Where } A = (\alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6)$$

$$B = (\alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6 + \beta_1)$$

$$C = (\alpha_2 + \alpha_3 + \alpha_4 + \alpha_5 + \alpha_6)$$

$$E = \beta_1 / (A-C)$$

$$A_0 = P_0 + P_1$$

$$A_0 = 1 / (1 + FG + H) + F / (1 + FG + H)$$

$$A_0 = P_0 (1 + F)$$

Decision Matrix for Filler System (Conveyer belt speed):

$\alpha_1 \backslash \beta_1$	0.00017	0.00018	0.00019	0.00020	0.00021	Constant Values
0.01	0.9749	0.9749	0.9749	0.9748	0.9748	$\alpha_2=0.00013, \beta_2=0.05$ $\alpha_3=0.00023, \beta_3=0.02$ $\alpha_4=0.00025, \beta_4=0.04$ $\alpha_5=0.00019, \beta_5=0.06$ $\alpha_6=0.00011, \beta_6=0.05$
0.02	0.9751	0.9751	0.9751	0.9751	0.9751	
0.03	0.9752	0.9752	0.9752	0.9752	0.9752	
0.04	0.9752	0.9752	0.9752	0.9752	0.9752	
0.05	0.9752	0.9752	0.9752	0.9752	0.9752	

Decision Matrix for Filler System (Sensors Assembly):

$\alpha_2 \backslash \beta_2$	0.00011	0.00012	0.00013	0.00014	0.00015	Constant Values
0.03	0.9741	0.9738	0.9735	0.9732	0.9728	$\alpha_1=0.00019, \beta_1=0.02$ $\alpha_3=0.00023, \beta_3=0.02$ $\alpha_4=0.00025, \beta_4=0.04$ $\alpha_5=0.00019, \beta_5=0.06$ $\alpha_6=0.00011, \beta_6=0.05$
0.04	0.9750	0.9747	0.9745	0.9743	0.9740	
0.05	0.9755	0.9753	0.9751	0.9749	0.9747	
0.05	0.9758	0.9757	0.9755	0.9754	0.9752	
0.07	0.9761	0.9760	0.9758	0.9757	0.9756	

Decision Matrix for Filler System (Star Infeed Wheel):

$\alpha_3 \backslash \beta_3$	0.00021	0.00022	0.00023	0.00024	0.00025	Constant Values
0.01	0.8170	0.8104	0.8038	0.7974	0.7911	$\alpha_1=0.00019, \beta_1=0.02$ $\alpha_2=0.00013, \beta_2=0.05$ $\alpha_4=0.00025, \beta_4=0.04$ $\alpha_5=0.00019, \beta_5=0.06$ $\alpha_6=0.00011, \beta_6=0.05$
0.02	0.8936	0.8897	0.8857	0.8818	0.8779	
0.03	0.9225	0.9197	0.9169	0.9141	0.9113	
0.04	0.9376	0.9354	0.9333	0.9311	0.9289	
0.05	0.9470	0.9452	0.9434	0.9416	0.9398	

Decision Matrix for Filler System (Rotary Filler):

$\alpha_4 \backslash \beta_4$	0.00023	0.00024	0.00025	0.00026	0.00027	Constant Values
0.02	0.9667	0.9663	0.9658	0.9653	0.9649	$\alpha_1=0.00019, \beta_1=0.02$ $\alpha_2=0.00013, \beta_2=0.05$ $\alpha_3=0.00023, \beta_3=0.02$ $\alpha_5=0.00019, \beta_5=0.06$ $\alpha_6=0.00011, \beta_6=0.05$
0.03	0.9703	0.9700	0.9697	0.9694	0.9691	
0.04	0.9721	0.9719	0.9717	0.9714	0.9712	
0.05	0.9732	0.9730	0.9728	0.9727	0.9725	
0.06	0.9739	0.9738	0.9736	0.9735	0.9733	

Decision Matrix for Filler System (Rotary Cork Attachment):

$\alpha_5 \backslash \beta_5$	0.00017	0.00018	0.00019	0.00020	0.00021	Constant Values
0.04	0.9736	0.9733	0.9731	0.9728	0.9726	$\alpha_1=0.00019, \beta_1=0.02$ $\alpha_2=0.00013, \beta_2=0.05$ $\alpha_3=0.00023, \beta_3=0.02$ $\alpha_4=0.00025, \beta_4=0.04$ $\alpha_6=0.00011, \beta_6=0.05$
0.05	0.9744	0.9742	0.9740	0.9738	0.9736	
0.06	0.9749	0.9747	0.9746	0.9744	0.9743	
0.07	0.9753	0.9751	0.9750	0.9749	0.9747	
0.08	0.9756	0.9754	0.9753	0.9752	0.9751	

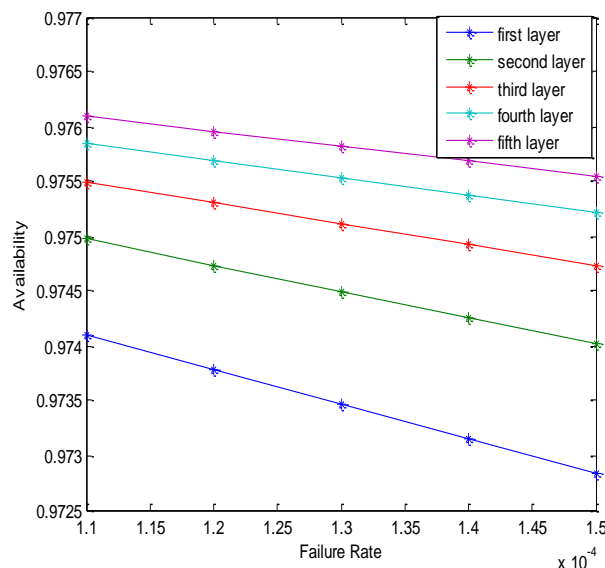
Decision Matrix for Filler System (Conveyer Belt):

$\alpha_6 \backslash \beta_6$	0.00009	0.00010	0.00011	0.00012	0.00013	Constant Values
0.03	0.9744	0.9740	0.9737	0.9734	0.9731	$\alpha_1=0.00019, \beta_1=0.02$ $\alpha_2=0.00013, \beta_2=0.05$ $\alpha_3=0.00023, \beta_3=0.02$ $\alpha_4=0.00025, \beta_4=0.04$ $\alpha_5=0.00019, \beta_5=0.06$
0.04	0.9751	0.9748	0.9746	0.9744	0.9741	
0.05	0.9755	0.9753	0.9751	0.9749	0.9747	
0.06	0.9758	0.9756	0.9755	0.9753	0.9751	
0.07	0.9760	0.9759	0.9757	0.9756	0.9754	

#### Analysis through Graph:

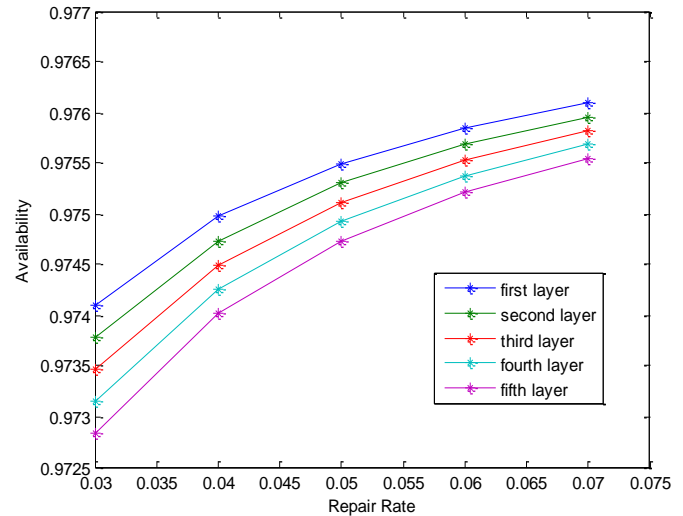
As we seen in the table the Availability changes as failure rate and repair rate changes. The most significant changes appears in Sensor Assembly the changes can be seen in the graphs below:

Graph A



Graph A: Failure Rate and Availability for Sensor Assembly

Graph B



Graph B: Repair Rate and Availability for Sensor Assembly

#### Conclusions:

The most critical sub-system of Filler system is "Sensor Assembly", the table and graphs shows the variation of availability with the change in failure rate and repair rate. As the value of failure rate increases from 0.00011 to 0.00015 the value of availability decreases but as we increase the value of repair rate from 0.01 to 0.05 the value of availability is increases nearly by 0.2 to 0.5%.

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